

ELEN E3401: Electromagnetics

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Lecture #16



COLUMBIA | ENGINEERING
The Fu Foundation School of Engineering and Applied Science



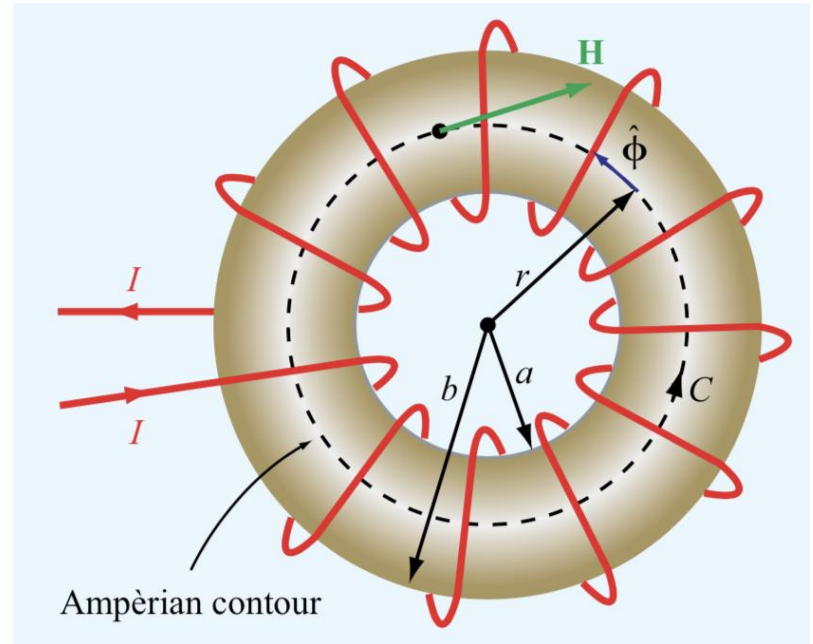
Magnetic Field of Toroid

Applying Ampere's law over contour C

$$\oint_C \vec{H} \cdot d\vec{l} = I$$

Ampere's law: the line integral of \vec{H} around a closed contour C is equal to the current traversing the surface bounded by the contour.

What's the magnetic field outside the toroid?



$$\oint_C \vec{H} \cdot d\vec{l} = \int_0^{2\pi} (-\hat{\phi}H) \cdot \hat{\phi} r d\phi = -2\pi r H = -NI$$

$$\text{Hence, } H = -\frac{NI}{2\pi r} \text{ and } \vec{H} = -\hat{\phi}H = -\hat{\phi} \frac{NI}{2\pi r} \text{ for } a < r < b$$

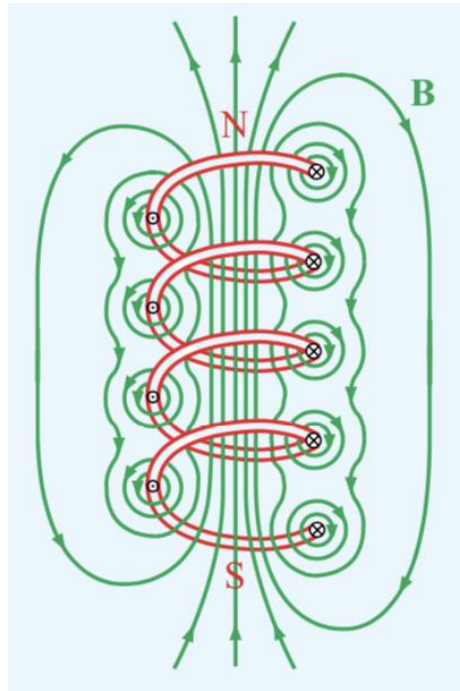
Inductance

Inductance \rightarrow analog of capacitance

Capacitor can store energy in \vec{E} field between conducting surfaces

Inductor stores energy in \vec{H} field near current carrying conductors

Solenoid



Multiple turns of wire – core can be air or magnetic material, μ

If turns are closely spaced

\rightarrow magnetic field can be uniform

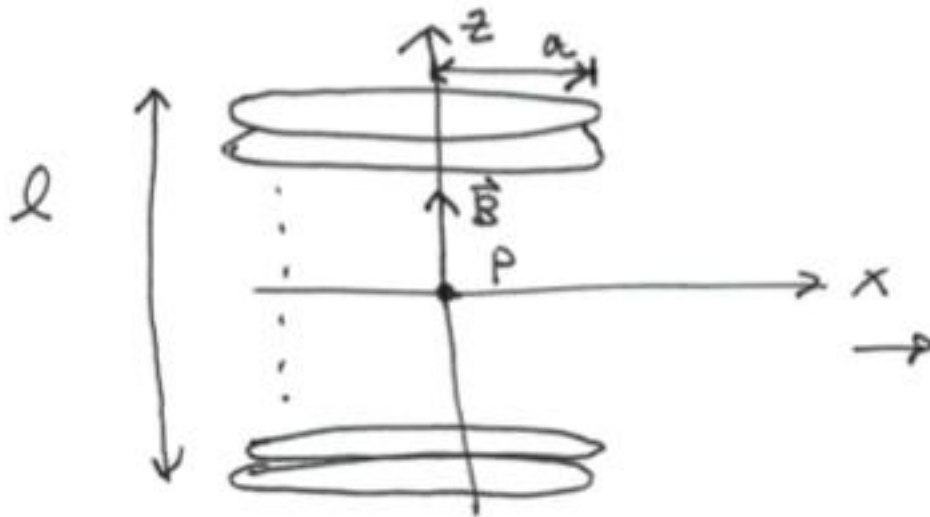
\rightarrow looks more like permanent magnet

Magnetic Flux in Solenoid

Tightly wound solenoid of length = l

Number of turns / unit length: $n = \frac{N}{l}$

because tight wound, treat helical shape as rings

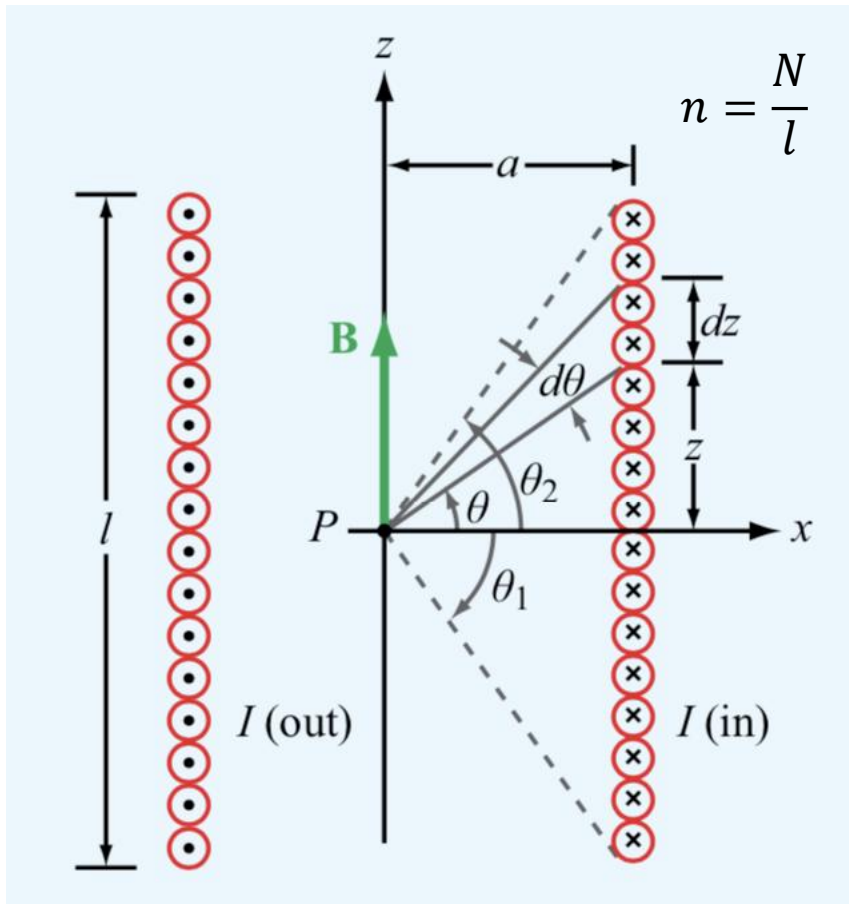


Radius = a

Length = l

Consider \vec{B} at point P on axis

Solenoid



We previously obtained magnetic field, \vec{H} along axis for 1 loop of current:

$$\vec{H} = \hat{z} \frac{I' a^2}{2(a^2 + z^2)^{3/2}}$$

a = loop radius

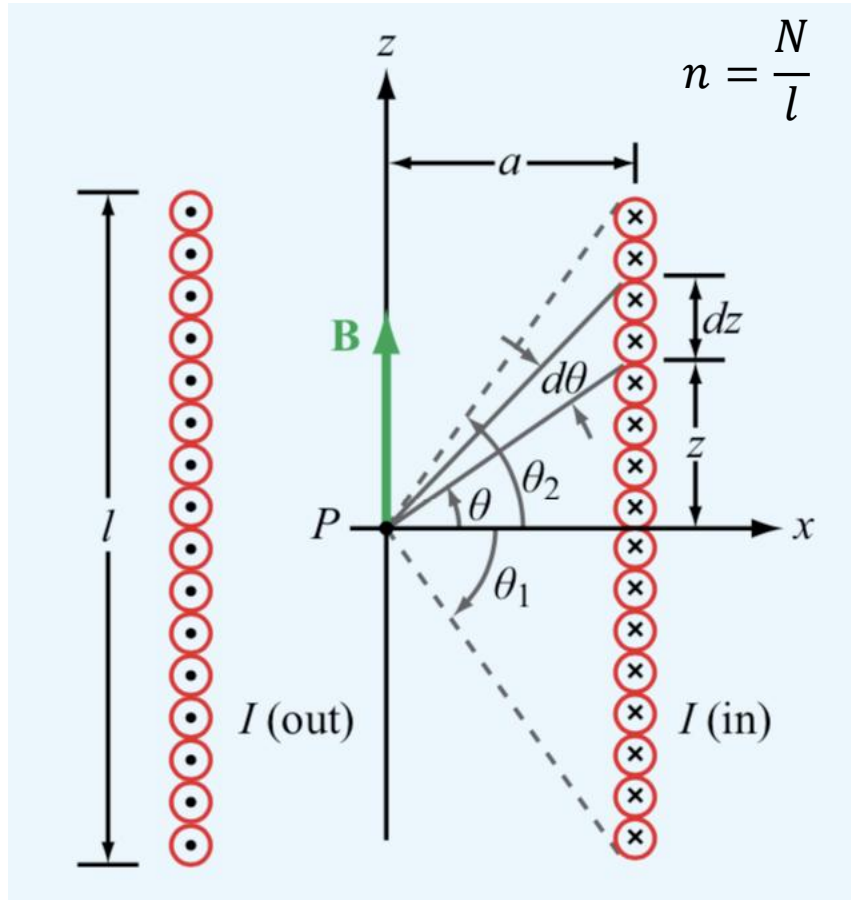
I' = current in loop

$$n = \frac{N}{l}$$

For solenoid:

dz of solenoid = equivalent to loop composed of (ndz) turns carrying current $I' = I(ndz)$

Solenoid



Then, at P :

$$I' = Indz$$

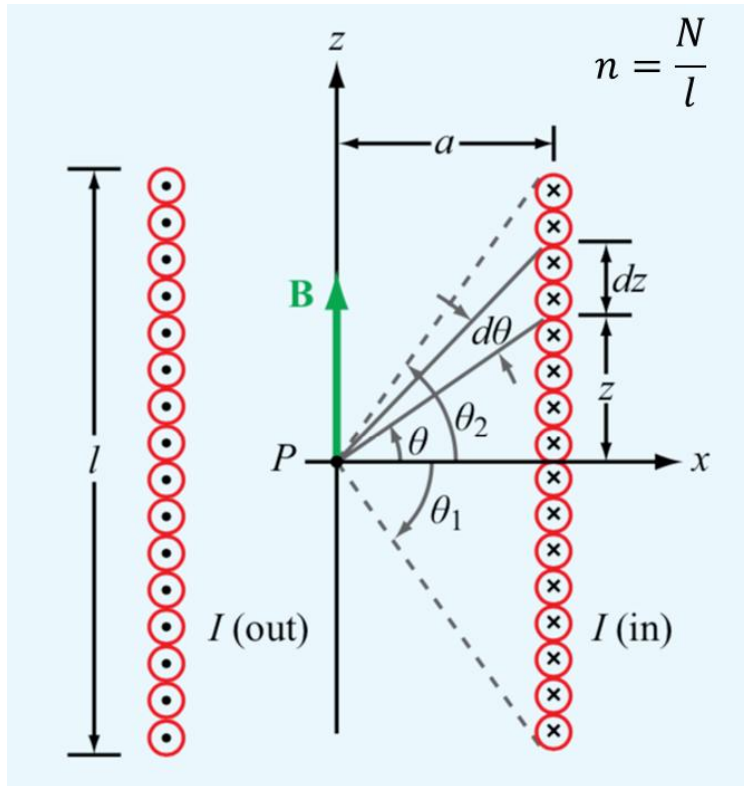
$$d\vec{B} = \mu d\vec{H} = \hat{z} \frac{\overbrace{\mu n I a^2}}{2(a^2 + z^2)^{3/2}} dz$$

Total \vec{B} : integrate over length of solenoid to compute \vec{B} as seen at P

Angle θ : angle as seen from P of solenoid

$$z = (a) \tan \theta \leftarrow \tan \theta = \frac{z}{a}$$

Solenoid



$$d\vec{B} = \mu d\vec{H} = \hat{z} \frac{\mu n I a^2}{2(a^2 + z^2)^{3/2}} dz$$

$$z = (a) \tan \theta$$

$$a^2 + z^2 = a^2 + a^2 \tan^2(\theta) = a^2 \sec^2 \theta$$

$$a^2 (1 + \tan^2(\theta))$$

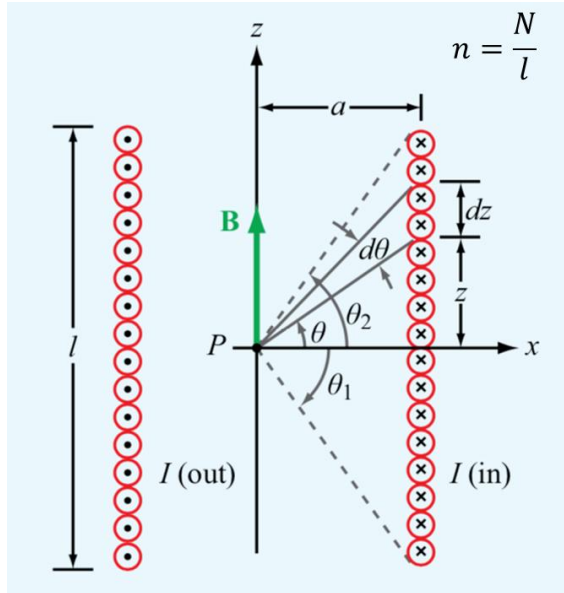
$$dz = a \sec^2 \theta d\theta$$

$$d\vec{B} = \mu d\vec{H} = \hat{z} \frac{\mu n I a^2}{2(a^2 + z^2)^{3/2}} dz$$

$$\vec{B} = \hat{z} \frac{\mu n I a^2}{2} \int_{\theta_1}^{\theta_2} \frac{a \sec^2 \theta d\theta}{a^3 \sec^3 \theta} \left. \begin{array}{l} \} = dz \\ \} = (a^2 + z^2)^{3/2} \end{array} \right\}$$

$$\vec{B} = \hat{z} \frac{\mu n I}{2} (\sin \theta_2 - \sin \theta_1)$$

Solenoid



$$\vec{B} = \hat{z} \frac{\mu n I}{2} (\sin \theta_2 - \sin \theta_1)$$

If solenoid length $l \gg a$, then $\theta_1 = -\theta_2 \approx \pm 90^\circ$ $\theta_1 \approx -90^\circ$ $\theta_2 \approx 90^\circ$

$$\vec{B} \approx \hat{z} \mu n I = \frac{\hat{z} \mu N I}{l} \quad \text{Long solenoid } l/a \gg 1$$



Holds for \vec{B} everywhere inside solenoid (except for ends)

Inductance

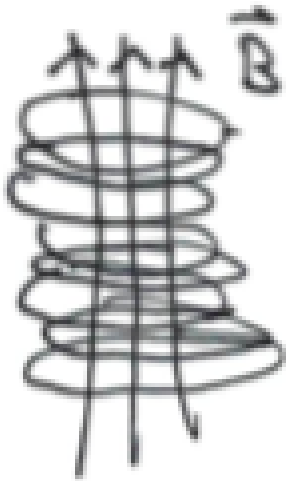
Self inductance: magnetic flux linkage of a coil (or circuit) with itself

Mutual inductance: magnetic flux linkage in a circuit due to magnetic field generated by a current in another circuit

Usually “inductance” refers to self inductance

Magnetic Flux and Magnetic Flux Linkage

Magnetic flux, Φ linking a surface S as magnetic flux density passing through surface:



$$\Phi = \int_S \vec{B} \cdot d\vec{s} \text{ [Wb]}$$

Solenoid with approximately uniform magnetic field through cross-section:

$$\vec{B} = \frac{\hat{z}\mu NI}{l} \quad l/a \gg 1$$

Magnetic flux

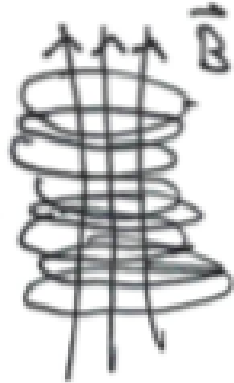
Flux linking single loop: $\Phi = \int_S \frac{\hat{z}\mu NI}{l} \cdot \hat{z}ds = \frac{\mu N}{l} IS$

Cross section area of loop

(Note: In the original image, the terms \vec{B} and $d\vec{s}$ in the integral are circled in red, and a blue arrow points from the text 'Cross section area of loop' to the IS term in the final part of the equation.)

Magnetic Flux and Magnetic Flux Linkage

Magnetic flux, Φ linking a surface S as magnetic flux density passing through surface:



$$\Phi = \int_S \vec{B} \cdot d\vec{s} \text{ [Wb]} \quad \vec{B} = \frac{\hat{z}\mu NI}{l}$$

Magnetic flux

Flux linking single loop:
$$\Phi = \int_S \frac{\hat{z}\mu NI}{l} \cdot \hat{z}ds = \frac{\mu N}{l} IS$$

Magnetic flux linkage: $\Lambda = N\Phi$

Total magnetic flux linking circuit or conducting structure

For solenoid structure: single conductor with multiple loops:

Magnetic Flux Linkage: $\Lambda =$ flux linking all loops of structure

Solenoid with N turns:
$$\Lambda = N\Phi = \frac{\mu N^2}{l} IS \text{ [Wb]}$$

Self Inductance

Self-inductance of any conducting structure:

Ratio of: (magnetic flux linkage) / (current flowing through structure)

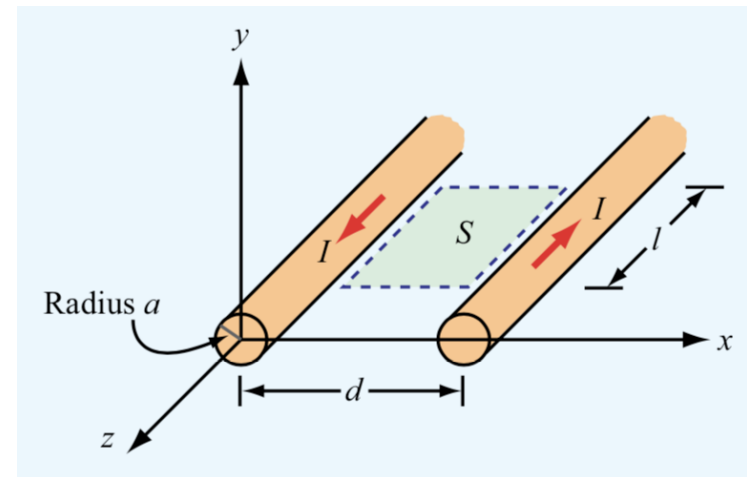
$$L = \frac{\Lambda}{I} \quad [H \text{ or } Wb/A]$$

For solenoid: $L = \frac{\mu N^2}{l} S \quad [H]$

For 2-conductor:

$$\Lambda = N\Phi = \Phi \rightarrow N = 1 \text{ (no turns)}$$

$$L = \frac{\Lambda}{I} = \frac{\Phi}{I} = \frac{1}{I} \int_S \vec{B} \cdot d\vec{s}$$

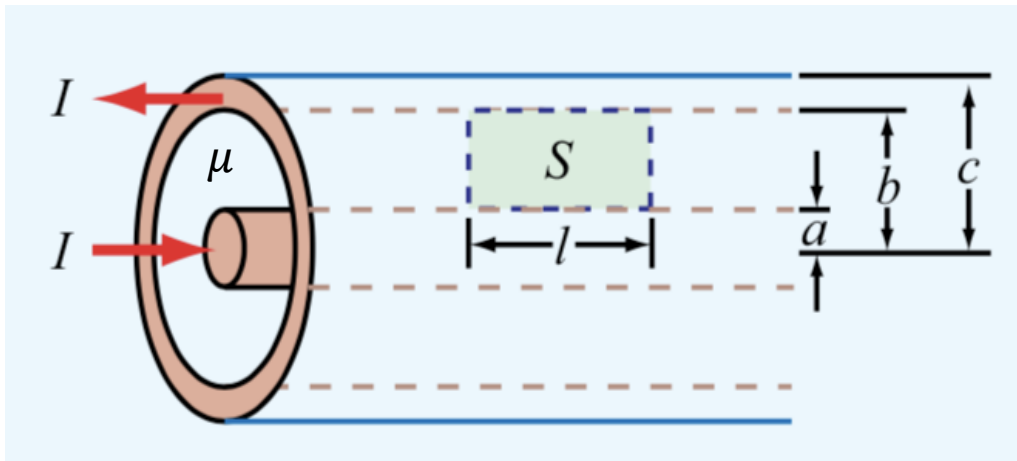


Example: inductance of coax transmission line

Obtain inductance per unit length of a coax transmission line:

Inner/outer conductors of radii a and b

Insulating material of permeability μ



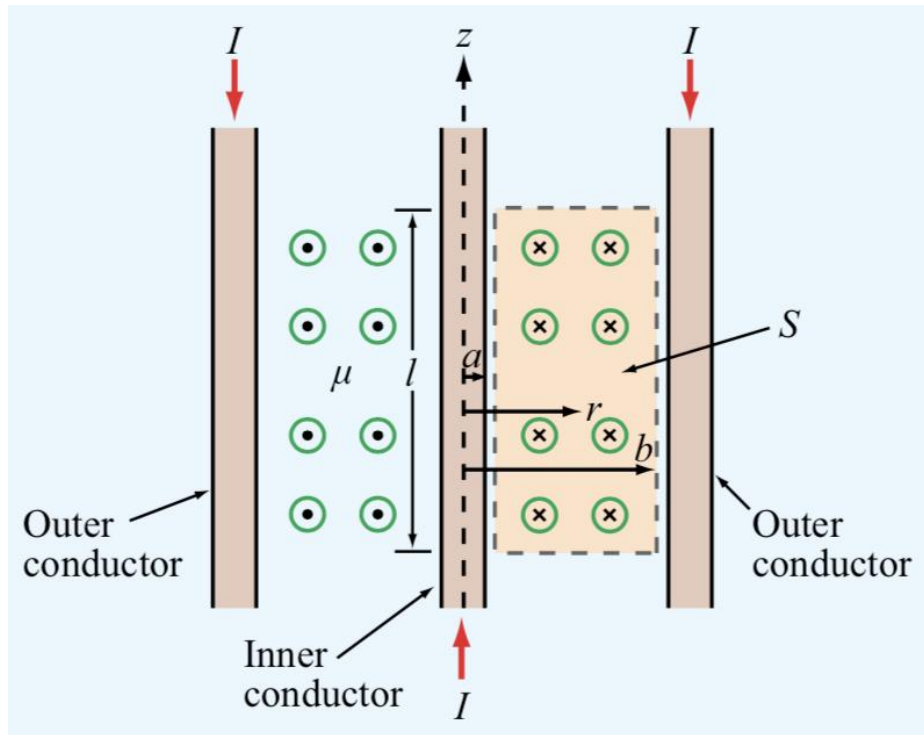
I in inner conductor generates \vec{B} in region between conductors:

$$\vec{B} = \hat{\phi} \frac{\mu I}{2\pi r} \quad r = \text{radial distance}$$

current is on outside surface of inner conductor and inside surface of outer conductor

Example: inductance of coax transmission line

Cross-section



$$\vec{B} = \hat{\phi} \frac{\mu I}{2\pi r} \quad r = \text{radial distance}$$

Considering a segment of the TL length l

\vec{B} is perpendicular to S , flux through S :

$$\Phi = l \int_a^b B dr = l \int_a^b \frac{\mu I}{2\pi r} dr$$

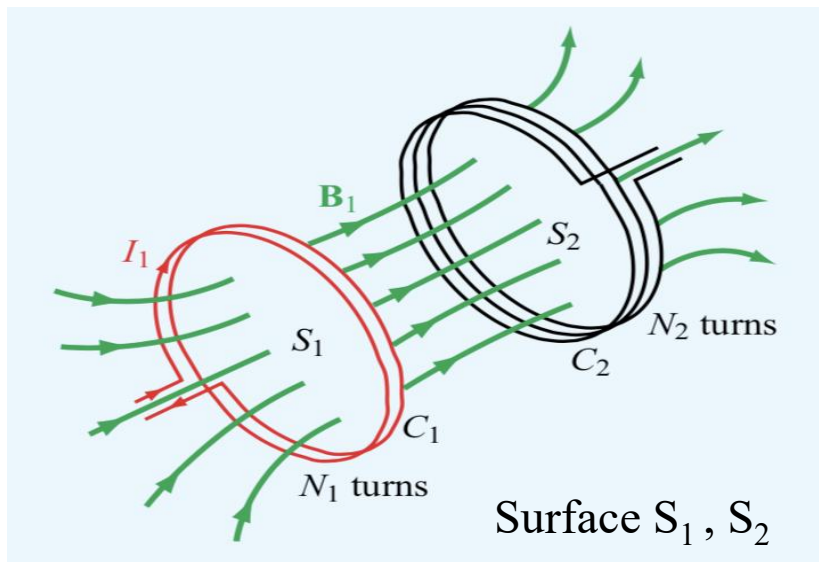
$$\Phi = \frac{\mu I l}{2\pi} \ln \left(\frac{b}{a} \right)$$

$$L' = \frac{\text{inductance}}{\text{unit length}} = \frac{L}{l} = \frac{\Phi}{Il} = \frac{\mu}{2\pi} \ln \left(\frac{b}{a} \right) \quad \left. \vphantom{\frac{\mu}{2\pi} \ln \left(\frac{b}{a} \right)} \right\} \text{Ch.2 Table 2-1}$$

Mutual Inductance

Magnetic coupling between 2 different conducting structures

Consider simple example of 2 multi-turn loops:



I_1 flows in Loop #1, no current in loop #2

\vec{B}_1 generated by $I_1 \rightarrow$ results in flux Φ_{12} through loop #2

$$\Phi_{12} = \int_{S_2} \vec{B}_1 \cdot d\vec{s}$$

If Loop #2 has N_2 turns, all coupled in same way, total magnetic flux linkage:

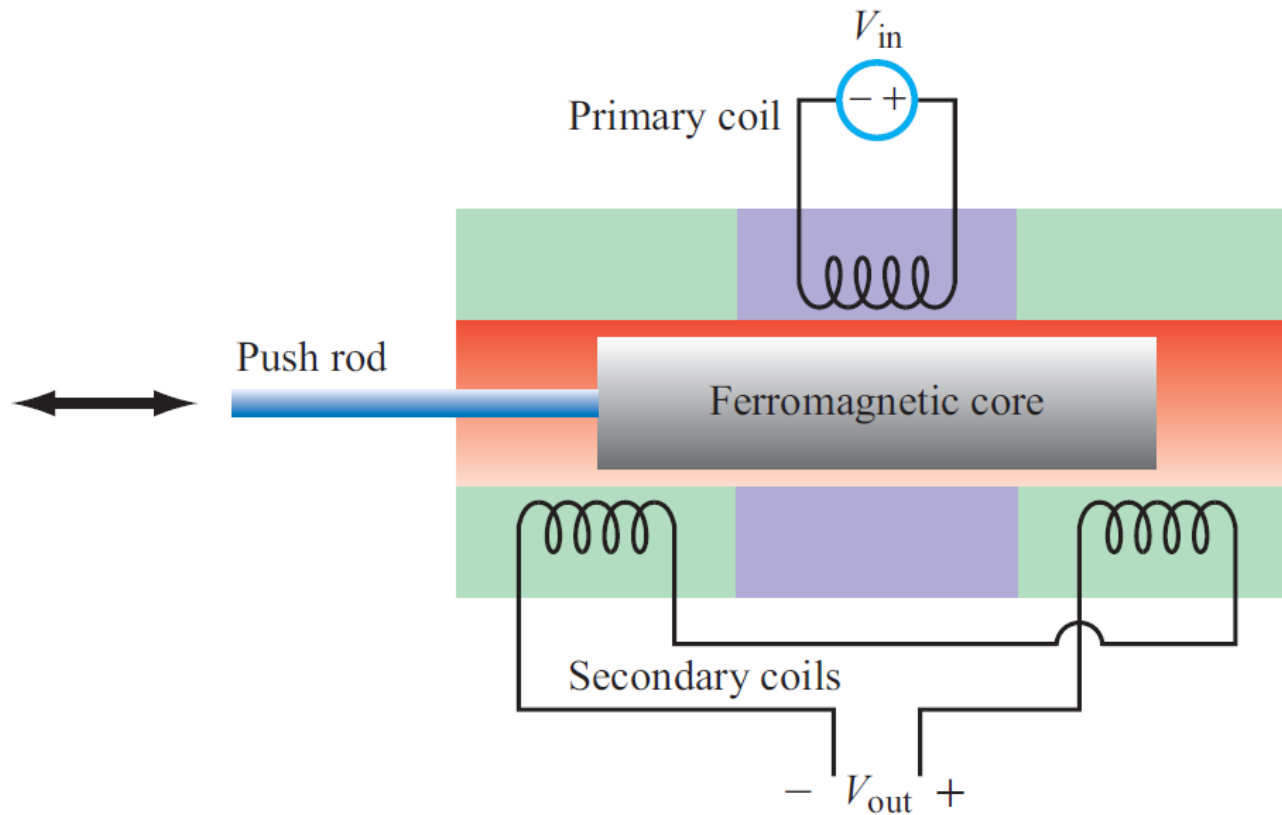
$$\Lambda_{12} = N_2 \Phi_{12} = N_2 \int_{S_2} \vec{B}_1 \cdot d\vec{s}$$

Mutual inductance:
$$L_{12} = \frac{\Lambda_{12}}{I_1} = \frac{N_2}{I_1} \int_{S_2} \vec{B}_1 \cdot d\vec{s}$$

important for transformers

Inductive Sensors

LVDT (linear variable differential transformer)
can measure displacement with submillimeter precision



Dynamic Fields

Reference	Differential Form	Integral Form
Gauss's law	$\nabla \cdot \mathbf{D} = \rho_v$	$\oint_S \mathbf{D} \cdot d\mathbf{s} = Q \quad (6.1)$
Faraday's law	$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$	$\oint_C \mathbf{E} \cdot d\mathbf{l} = -\int_S \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{s} \quad (6.2)^*$
Gauss's law for magnetism	$\nabla \cdot \mathbf{B} = 0$	$\oint_S \mathbf{B} \cdot d\mathbf{s} = 0 \quad (6.3)$
Ampère's law	$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$	$\oint_C \mathbf{H} \cdot d\mathbf{l} = \int_S \left(\mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} \right) \cdot d\mathbf{s} \quad (6.4)$
*For a stationary surface S .		

We will be focusing on Faraday's and Ampère's laws